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Foth & Van Dyke

**Groundwater Withdrawal Permit
Application for the
Kennecott Flambeau Project**

Scope I.D.: 87K10

*Kennecott Minerals Company
Ladysmith, Wisconsin*

April 1989



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April 1, 1989

Kennecott

Mr. Roger Gerhardt
Private Water Section
Wisconsin Department of Natural Resources
P. O. Box 7921
Madison, WI 53707

87K10-57

Dear Mr. Gerhardt:

RE: Groundwater Withdrawal Permit Application
Kennecott Flambeau Project

Kennecott Minerals Company (Kennecott) is submitting a groundwater withdrawal Application Permit for its Flambeau open pit mining project, located approximately 1.6 miles south of Ladysmith on STH 27. Groundwater will be withdrawn to dewater the mine pit and will also be withdrawn through existing wells and a new potable water well.

Pursuant to discussions with representatives of the Department, this permit is being submitted under Wis. Stat. s. 144.855(3), which the Department maintains requires that groundwater withdrawal be approved under Wis. Stat. s. 144.025(2)(e), the so-called high capacity well provisions. Obviously, many of the technical requirements for high capacity wells are not applicable to dewatering an open pit mine. Nevertheless, at the Department's request we have attempted to apply the provisions of Wisconsin Administrative Code ch. NR 112 where possible. Reference will be made to the Environmental Impact Report and Mining Permit Application where appropriate. A general description of the project is also enclosed.

As per an agreement developed with the Department, it is our understanding that the WDNR will distribute this application to all appropriate state and federal agencies. Kennecott will distribute the document to appropriate local public officials.

Kennecott is requesting that the WDNR review this application as expeditiously as possible such that permitting activities associated with the project can continue in a timely manner.

Mr. Roger Gerhardt
Wisconsin Department of Natural Resources
April 1, 1989
Page 2

If you have any questions regarding this application please contact Gerald W. Sevick, P.E. at (414)497-2500 or myself. Mr. Sevick is an engineer with Foth & Van Dyke and Associates Inc., Green Bay, Wisconsin, Kennecott's consultant for this project.

Sincerely,

KENNECOTT

Lawrence E. Mercado

Lawrence E. Mercado
Director, Process Development

Enclosures

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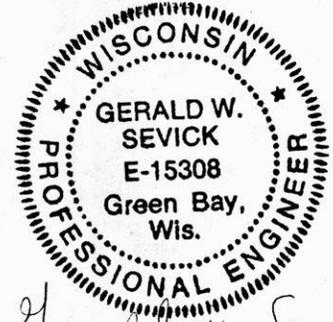
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GROUNDWATER WITHDRAWAL
PERMIT APPLICATION
FOR THE
KENNECOTT FLAMBEAU PROJECT



Gerald W. Sevick
4/1/89

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APRIL 1989

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Based on 1983 Model Simulations

1.0 DESCRIPTION OF THE PROPOSED PROJECT

1.1 Introduction

The project facilities will consist of an open pit mine; an unlined (Type I) stockpile for storage of overburden, saprolite, sandstone, and waste rock containing very low levels of sulfide mineralization; a lined (Type II) stockpile for storage of saprolite and waste rock containing slightly higher levels of sulfide mineralization; a topsoil stockpile; water control features; a wastewater treatment plant; and ancillary facilities such as an office, railroad spur line, and maintenance building.

Figure No. 1 has been prepared to graphically illustrate the proposed project. The figure is a plan view of the mine area showing the location and relative size of key project elements.

1.2 Geology

1.2.1 Description of Site Geology

Precambrian volcanic rock, Cambrian sandstone, and Quaternary glacial and fluvial sediments are present beneath the project area. The geology has been defined from hundreds of soil borings and core samples drilled on site and from scattered outcrops along the banks of Meadowbrook Creek.

The steeply dipping Precambrian rock has been highly altered during mountain building processes to schist, which was later weathered and further altered. The top ten to 20 feet of Precambrian waste rock has been weathered to a silty-clay rock termed saprolite.

Small amounts of disseminated pyrite have been oxidized below the saprolite to several tens of feet in depth. This rock is termed Type I waste rock and contains less than one percent sulfur. Type I material has been leach column-tested and found to produce water of quality that can be discharged without treatment. Type II waste rock occurs in the lower levels of the proposed open pit. Because this material contains greater than one percent sulfur, it will be stored on a lined stockpile area.

The Precambrian rock is overlain by Cambrian sandstone which consists of a poorly cemented, fine to coarse-grained quartz sand. Thickness of the sandstone varies from zero to greater than 30 feet within the proposed pit perimeter.

Near-surface materials consist of unconsolidated Quaternary glacial-fluvial sediments. Most of the deposit is covered by a dense, silty-sand glacial till. Glacial-fluvial sand and gravel generally occur in the northwest part of the project area in the vicinity of the abandoned gravel pit.

1.2.2 Deposit Description

The Flambeau deposit is tabular in shape, strikes in a northeast direction, and dips steeply to the northwest. The upper portion of the sulfide mineralization has been enriched in copper as a result of ancient fluctuating groundwater tables to about 225 feet below the present land surface. The deposit to be mined is 2,600 feet long, averages 50 feet wide, and contains approximately 1.9 million tons of material. The upper part of the deposit consists of zero to 30 feet of iron oxide-rich gossan. Below the gossan are varying proportions of chalcocite and bornite (copper sulfide minerals) in a matrix of chert (cryptocrystalline quartz) and pyrite (iron sulfide). No significant or economic amounts of sulfide mineralization have been found by drilling in either direction from the deposit. Sulfide

mineralization occurring beneath the proposed pit has been determined by Kennecott to be uneconomical based upon projected metal prices.

1.3 Description of Key Project Elements

1.3.1 General Mine Plan

Enriched ore will be mined from an oval-shaped open pit designed to cover approximately 32 acres to a maximum pit depth of 225 feet. All excavated materials will be hauled to the surface, which is at about 1,140 feet Mean Sea Level. Ore will be transported by truck to a crushing facility adjacent to the pit and crushed to minus 12 inches for rail shipment to an out-of-state processing facility.

Two open pit mining phases will be used. The first will mine the southwest half of the deposit to the 970-foot elevation. The second mines the balance of the pit to its final lateral limits and extends the pit bottom to the 900-foot elevation. Due to variation in the orebody grades, two ore-mining faces will be available at all times. Hydraulic shovels will operate from 20-foot high benches. The next bench is prepared as soon as working room becomes available to allow for construction of a sump to handle in-pit water flows and for emergency storage during heavy precipitation.

Waste material will be classified in the pit by sulfur content and stored on either lined or unlined storage sites adjacent to the pit. Eventually waste materials from the separate stockpiles will be returned to the pit as backfill. Upon completion of the mining operation, the project site will be contoured and reclaimed. Land owned by Kennecott but not included in the project area will mostly remain in its current use.

1.3.2 Mining Operation

Preproduction activities will take approximately 10 months to develop the open pit, the waste rock stockpiles, and plant facility. Chief tasks will be clearing the site; preproduction stripping; construction of access roads, the railroad spur, powerline, wastewater treatment plant, storage areas, etc. Disturbed soil areas will be stabilized and water control measures installed at that time.

The Flambeau orebody will be mined from the open pit over a period of approximately six years. The pit area at the end of the mine life will embrace an oval-shaped area of approximately 32 acres. The pit will be 2,600 feet long and average about 550 feet wide. Open pit mining will take place five to six days a week, eight hours per day, to produce approximately 320,000 dry short tons of ore per year.

The steeply dipping rocks will accommodate a pit, with slopes at 36° for the glacial till and 50° interramp for rock sections. Twenty-seven-foot wide catch benches will be left at 60-foot intervals for safety considerations. The access ramp has a design width of 60 feet and a gradient of ten percent.

Overburden, ore, and waste rock will be excavated from 20-foot high benches using conventional mining equipment. The excavated overburden will be transported to the Type I stockpile or to construction areas elsewhere on the project site.

It is anticipated that most of the Cambrian sandstone, all of the saprolite and some of the oxidized waste rock (Type I) can be broken by using a dozer with a ripper blade. However, certain areas of the deposit, such as those portions of the orebody that contain quartz or hard waste rock, will require drilling and blasting. Fresher and harder rock and ore can be expected as the open pit deepens during the first year of full

production. Therefore, blasting during preproduction and into the first year of production will likely be performed only on an infrequent basis.

Controlled blasting procedures will be used to minimize the generation of seismic waves and noise. Due to the small scale of the mining method and operations, ore blasts will be relatively small. Blasting is anticipated to occur from one to five times per week. A set of blasting standards will be carefully followed to keep risks of flyrock, ground vibrations, and noise to a minimum.

Two four-cubic yard shovels and a seven-cubic yard loader will be used to load the broken ore and other materials into 35-ton or 50-ton trucks. At first, only four trucks will be required. The truck fleet will be increased to a maximum of seven trucks as the pit deepens and haul distance increases. A 4,000-gallon water truck will wet haul roads and truck unloading areas for dust control.

Anticipated production and operation schedules are found in Table No. 1-1. The tonnages shown in the table are averages since ore and spoils production vary from year to year.

TABLE NO. 1-1

Anticipated Production and Operation Data

Preproduction Stripping	1,500,000 tons
Daily Ore Production	1,300 tons
Annual Ore Production	320,000 tons
Total Ore Production	1,900,000 tons
Total Overburden & Waste Rock	8,000,000 tons
Total Material Moved (Includes Backfill)	17,500,000 tons
Open Pit Size	32 acres
Project Area	300 acres
Total Project Life	8 to 9 years
Preproduction and Construction	1 year
Mining	6 years
Rehabilitation & Backfilling	1 to 2 years
Open Pit Operating Schedule	5 to 6 days/week 8 hours/day, 1 shift
Crushing Plant	5 to 6 days/week 8 hours/day, 1 shift
Employment During Operations	
Initial	56
Peak	61
Average	55

1.3.3 Water Inflow Controls

When topsoil is stripped and excavation begins, control methods will be provided for surface water and groundwater that could flow into the open pit. Hydrologic studies indicate that a simple system of grading and ditching to a series of sumps can

capture and control most of the water expected to inflow. The water will then be diverted to settling ponds or to the wastewater treatment plant. A slurry wall of either grout or bentonite clay will be constructed at the end of the pit adjacent to the river to minimize potential inflow from that direction. Detailed geologic mapping will be routinely conducted to identify, monitor, and control any areas of significant water inflow which might develop.

Two water collection systems are planned for the pit. During preproduction stripping, an upper sump will catch surface and groundwater inflows from the glacial overburden and Cambrian sandstone. This water, which will not come into contact with sulfide mineralization, but which could carry suspended solids such as clays, will be pumped to settling ponds to remove suspended materials and colloids. The clear overflow will be used to provide water to an adjacent wetland or be discharged to the Flambeau River. A lower sump will collect all groundwater inflow and precipitation that comes into contact with ore and waste rock. Water from the lower sump will be pumped to the wastewater treatment plant, treated, and then separately discharged to the Flambeau River or an adjacent wetland.

A flood control dike will be constructed at the west end of the open pit to prevent overflow of the river into the pit during potential severe flooding conditions (100-year flood). The dike will be constructed using specially selected materials overlying the orebody. Rip rap protection will be installed on the river side of the dike. The west toe of the flood-control dike would be approximately 70 to 90 feet from the east edge of the current Flambeau River channel. The edge of the open pit will be no closer than 140 feet from the east edge of the river channel.

1.3.4 Crushing Facilities

The crushing facility consisting of a crusher, crushed ore stockpile, and railcar loading area will be built on the southwest side of the Type II waste rock stockpile. The crusher will be separated from the Type II stockpile by a retaining wall to contain rock and runoff water. The proximity of the crusher facility and stockpile to the pit minimizes haul distances. The crushing and ore loading areas will be contoured and underlain with a 60-mil HDPE liner to direct water to a runoff catchment pond for transfer to the wastewater treatment plant. All crushing will occur during daylight operations. The crusher will be oriented in a southwest direction to direct noise away from populated areas. The crusher is designed to crush coarse ore to minus 12 inches. A dust suppression spray system will control dust generated by the crusher and conveyor belt discharge point.

The crushing facility is designed for 250 tons per hour and allows for production variations and maintenance. Crushed and bypassed ore will be discharged onto a conveyor belt and transported to the crushed ore stockpile, where a front-end loader will load railroad cars at the rate of up to 20 to 24 cars per working day. It is planned to ship 15 to 24 loaded cars every other operating day.

1.3.5 Infrastructure

1.3.5.1 General

Several buildings will be erected to support the open pit operation and crushing plant. Chief infrastructure components will consist of a wastewater treatment plant, railroad spur, utilities, administrative building and shop, storage tanks, and explosives magazine. Most of these ancillary facilities will be clustered east of the crushing plant.

1.3.5.2 Wastewater Collection and Treatment Plant

The wastewater treatment plant, located southeast of the crushing facility, will be designed to treat water from four sources: 1) pit contact water, 2) ore haul road drainage, 3) Type II material storage pad drainage and runoff, and 4) site runoff from the crushing and loadout facilities and other ancillary facilities. Water from these combined sources will average approximately 617 gallons per minute on an annual basis.

A uniform feed of untreated wastewater to the treatment plant aids optimum plant performance. It is important, though, to consider surge capacity in its design, since water volume and metal loading can change with the seasons. Therefore, the wastewater treatment plant design provides for water storage in both a lined runoff catchment pond and a lined wastewater treatment surge reservoir. The open pit will also be used for emergency water storage. A 25-year rainfall event has been used as the design basis for the wastewater treatment system.

The wastewater treatment plant has been designed to process wastewater for acid neutralization and metal removal in a three-stage process. The process consists of lime treatment, sulfide precipitation, and mixed media filtration.

Sludge handling and treated water disposal make up the final components of the wastewater treatment system. Some of the treated water will be recycled for plant operations, makeup water, washdowns, and dust control with the balance discharged to the Flambeau River or an adjacent wetland. Sludge at approximately 25 percent solids will be trucked from the treatment plant to the Type II stockpile where it will be mixed with the stored waste rock.

1.3.5.3 Access Roads and Railroad Spur

Two access roads and a railroad spur will be constructed for the project. A new, paved plant site access road will be built from State Highway 27 into the project site. The road will be constructed opposite the intersection of Jansen Road and State Highway 27. A second access road to a visitors' observation platform is planned to be constructed approximately 2,700 feet north of the plant access road.

A single line railroad spur approximately 6,500 feet long will be constructed from the Wisconsin Central Ltd. railroad line southwesterly to the crusher plant site to provide access to railroad cars used for shipping ore. The spur line at the crusher plant site will consist of two parallel tracks for ease in loading and switching railroad cars. The primary route for the railroad spur is north of Jansen Road along a location which avoids as much of existing wetlands as possible.

1.3.5.4 Utilities

The electrical power supply for the Flambeau Project will be delivered at 13.8 Kv from the Northern States Power Company power grid to a main substation adjacent to the wastewater treatment plant. Natural gas will be extended to the site for space heating needs.

A low capacity potable water well will be drilled to supply water to field offices and shops.

1.3.5.5 Buildings and Shops

A maintenance shop, office building, and guard house will be erected south and east of the crushing plant. The existing utility building east of the pit will be used to house a limited inventory of equipment and supplies. A peripheral security

fence will be constructed around the entire plant site and open pit.

1.3.5.6 Mining Materials and Storage Tanks

Two portable magazines will be located in a remote bunkered area north of the Type I stockpile settling ponds. A blasting cap storage building will also be located in the same general area, but separated from the magazines. A 15,000-gallon diesel fuel tank and associated piping will be installed to provide fuel for mining equipment.

1.3.6 Solid Materials Stockpiles

Topsoil, overburden and Type I and Type II material will be removed and segregated in accordance with their characteristics, then stockpiled in the appropriate location for use in reclamation following the completion of mining.

1.3.6.1 Topsoil Stockpile

The top 12 to 18 inches of soil will be removed from all construction sites and placed in the topsoil stockpile. In some areas, such as the railroad spur cut and fill banks, access road slopes, and exposed berms, the topsoil will be moved to one side and then returned to stabilize and support temporary revegetation of these areas upon completion of construction. Topsoil from the open pit, crusher plant and excess topsoil from the storage areas will be removed and stockpiled. The topsoil stockpile area will be located east of the pit. This stockpile will serve as a visitors' viewing area. Stockpiled topsoil will be used to reclaim the site after mining activities are completed. The topsoil stockpile area will cover approximately seven acres.

1.3.6.2 Overburden/Type I Stockpile

Overburden and Type I material (less than one percent sulfur) will be stored on an unlined area located between the open pit and Blackberry Lane. A bermed swale at the base of the stockpile will contain internal runoff and direct it to the settling ponds. The stockpile will occupy about 40 acres, reach a height of about 60 feet, and have a design capacity of approximately 2.8 million cubic yards.

1.3.6.3 Type II Stockpile

Type II material (more than one percent sulfur) will be stockpiled separately in a lined area located southeast of the open pit and northeast of the crushing plant site. Approximately 27 acres will be required for this stockpile, which has been designed with a capacity of approximately 2.2 million cubic yards. The Type II stockpile will be built with an impervious liner and leachate collection system at its base. A lined berm and runoff containment swale will encircle the area to collect all precipitation that comes into contact with this material. Collected leachate and runoff will ultimately be directed via piping to the surge reservoir and then to the wastewater treatment plant.

Perimeter berms for the Type II stockpile will be constructed using overburden or soil excavated during base grade preparation. A protective layer of coarse-grained soils will be placed over the HDPE liner to protect the liner as waste rock is hauled onto the stockpile. The projected height of the stockpile is approximately 70 feet. The outside of the perimeter berm will be topsoiled and vegetated.

1.3.7 Surface Water Controls

As previously discussed, precipitation falling within the limits of the open pit, Type I and II storage piles, and plant area will be collected and directed to either the settling ponds or the wastewater treatment plant. Some of the surface water drainage originating from outside the active mine area will be intercepted by a series of drainage swales and directed to existing natural drainage features.

1.3.8 Reclamation

Disturbed soil areas will be revegetated and woodlands maintained during the life of the mining project. The open pit will be backfilled once mining is complete. The plan is to return the project site to as close to approximate original contours, such that it will be suitable for other land uses. Stockpiled Type II material will be placed at the bottom of the pit, with Type I waste rock placed over it and compacted as part of normal traffic of equipment used for backfilling. Saprolite, followed by sandstone and till will then be placed within the pit over the Type I waste rock. Finally, the pit site covered with topsoil and the area revegetated. Surface facilities, including the railroad spur, will be dismantled at the end of mine operations unless a beneficial plan for keeping all or some of the facilities is developed by Kennecott, the WDNR, and local residents.

2.0 SUPPLEMENTAL INFORMATION

Many of the technical requirements for high capacity wells are not applicable to dewatering an open pit mine. The following items address the potentially relevant factors of NR 112.26(1)(d):

2.1 Description of Property

The full legal description of the property including contiguous property owned by Kennecott is included in Section 2.0 of the Mining Permit Application. Figure No. 2 depicts the project area and ownership.

2.2 Owner and Operator

The owner of the property and facility is Kennecott Minerals Company, 1515 Mineral Square, Salt Lake City, Utah 84112. Lawrence E. Mercado, Director, Process Development, is the contact person at Kennecott Minerals Company. Kennecott will also own and operate all wells.

2.3 Existing Well Location

Figure No. 3 shows existing well locations both in the project area and on the adjacent property. Per discussions with the WDNR, the center of the open pit area has been used as the center of the 2500 foot radius to determine the location of those wells within 2500 feet of the "high capacity well." Also shown is the nearest public utility well owned by the City of Ladysmith. It should be noted that all wells located within the 2500 feet area are owned or controlled by Kennecott Minerals Company.

2.4 Existing Well Description and Water Use

Both the Wisconsin Department of Natural Resources (WDNR) private water section and the Wisconsin Geological and Natural History Survey have been contacted regarding the availability of well construction reports for wells around the project area. Unfortunately, these records were not complete. As a result, site visits were conducted to visually inspect the wells and question present owners. Those construction reports which could be identified with certainty with present or former property owners within the 2500 foot radius are contained in Appendix 3.6-F of the Environmental Impact Report. Table No. 2-1 summarizes the available data on existing well construction.

No records were available on water use, so water use was calculated based on occupancy. A 30 gallon per day per occupant use was assumed based on comparable water usage figures for wastewater treatment design. These figures are also noted in Table No. 2-1.

2.5 Proposed Water Use from New Sources

A high capacity pump will be used to control groundwater flows during Kennecott's mining operation. The range of flow will be approximately 294 gpm steady rate with a maximum flow of 588 gpm. The anticipated life of the entire mining operation will be approximately nine years.

A new potable water well will provide water to the employees at the site. The average flow for this domestic well will be approximately 1.8 gpm.

TABLE NO. 2-1

Kennecott Minerals Company
Flambeau Project
Existing Wells In Project Area

Well No.	Gal. Day*	Well Depth (ft.)	Date (1988) Water Level	Casing Diameter Inches	Pump Type	Groundwater Elevator
3	60	33	11/19 24.4	4	SUBM	1088.3
20	60	23	11/03 18	4	JET	1084.7
7	120	36	11/01 21.1	4	SUBM	1080.9
12	60	46	11/02 37.2	5	JET	1108.8
13	60	59	10/31 42.5	5	SUBM	1110.6
15	60	44	11/01 23.0	4	SUBM	1132.9
16	120	41.5	11/02 17.5	4	SUBM	1138.5
10A	120	48.3	10/31 40.4	5	SUBM	1114.9
18	---	36.8	11/02 8.0	5	SUBM	1138.2
21	---	45.6	11/02 12.6	4	SUBM	1132.2
22	150	49.3	10/31 13.5	5	SUBM	1132.5
23	60	37.8	11/03 13.3	5	SUBM	1133.7
70	120	24	10/31 15.3	4	SUBM	1137.2

*Assumes 30 g/d/capita

2.6 Construction of New Sources

See Section 3.5 of the EIR and Section 4.0 of the Mining Permit Application for pit geological and construction details. The potable water supply well will be constructed in accordance with NR 112.

2.7 Plan of Property

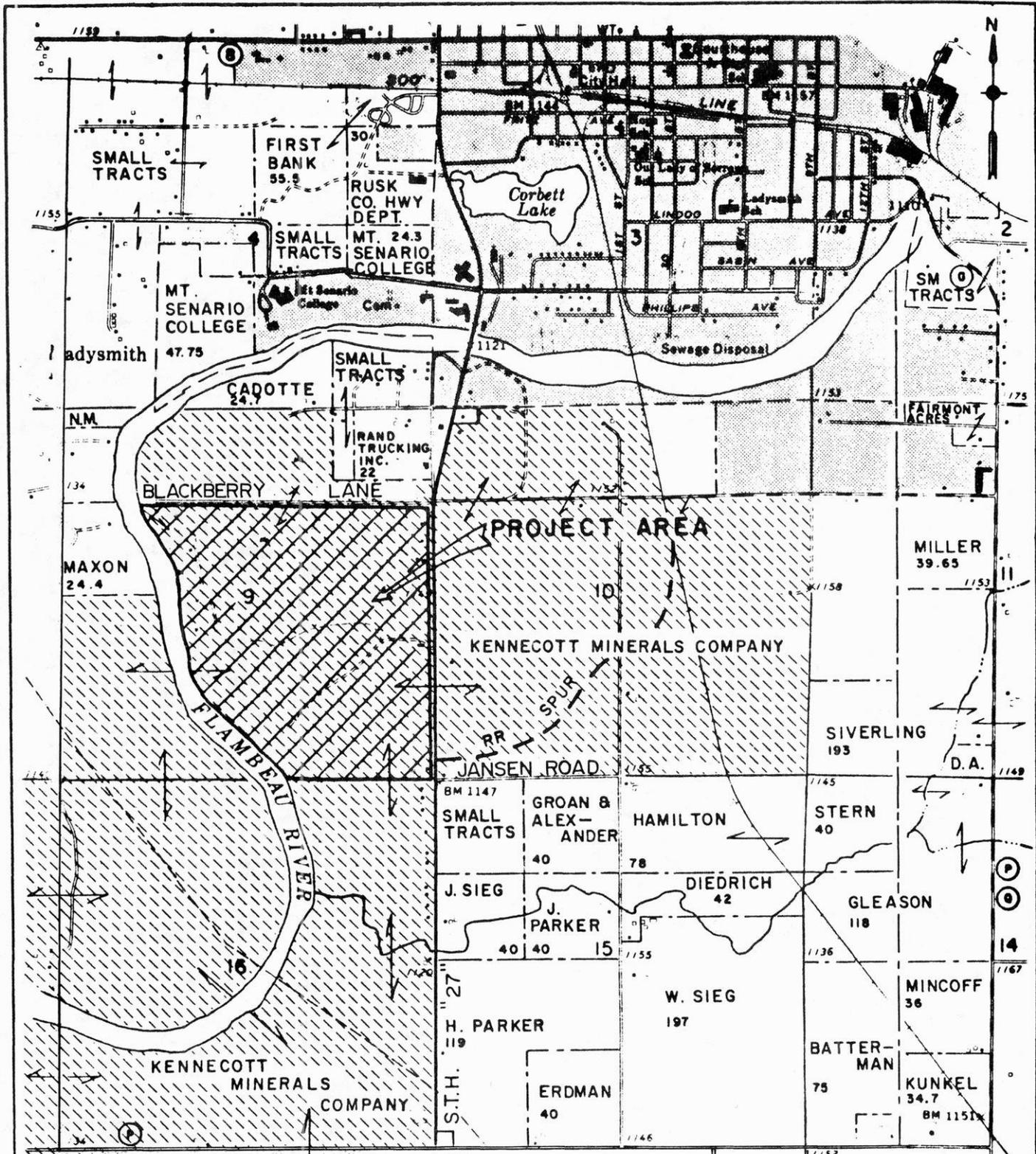
A plan of property showing location of buildings, wells, and possible contamination sources is shown on Figure No. 4 and is discussed in the Mining Permit Application.

2.8 Mine Dewatering Impacts

Figure No. 5 shows the maximum drawdowns that would have resulted if a mine plan proposed by Kennecott in 1975 had been implemented. This earlier mine plan involved an open pit that was deeper (285 verses 225 feet), larger in areal extent (55 verses 32 acres), and in existence for a much longer period of time (12, verses 5 years) than the currently proposed mine plan. Therefore, the currently proposed mine plan will place much less stress on the groundwater system and should result in a smaller area of maximum drawdown that that shown on Figure No. 5.

An implemented 1975 mine plan would have produced drawdowns in private wells only in the vicinity of STH 27 between Blackberry Lane and Jansen Road, an area in which all the private wells are owned by Kennecott. The most extreme drawdowns would have been only three to six feet, hardly more than normal seasonal fluctuations in water levels during an average year. The smaller extent of the current mine plan should produce drawdowns even less than those shown in Figure No. 5. Therefore, it is concluded that the drawdown to be produced by the mine as currently proposed will not significantly impact water levels in any private wells.

Figures for Permit Application

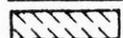
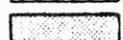


NOTES:

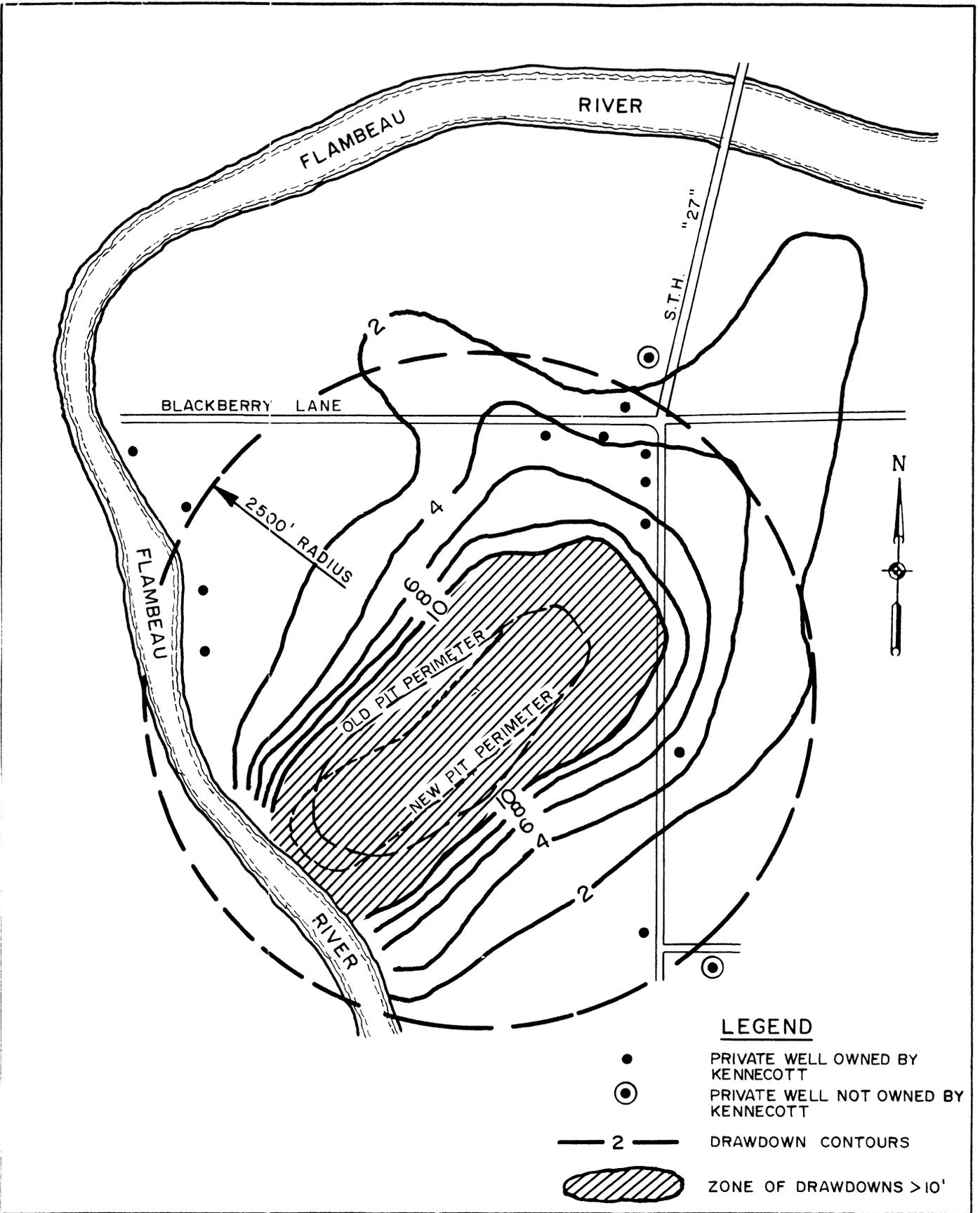
PROJECT AREA INCLUDES A 36 FOOT WIDE CORRIDOR ALONG RAILROAD SPURLINE EAST OF STH 27.

BASE MAP PREPARED FROM U.S.G.S. MAPS 7.5 MINUTE SERIES, LADYSMITH AND THORNAPPLE WI. QUADRANGLES

LEGEND

-  KENNECOTT PROPERTIES
-  CITY OF LADYSMITH

FOTH & VAN DYKE GEOSCIENCES & ENVIRONMENTAL MANAGEMENT DIVISION GREEN BAY, WISCONSIN			KENNECOTT MINERALS COMPANY FLAMBEAU PROJECT LADYSMITH, WISCONSIN		
NOTES	APPROVAL	DATE	FIGURE NO. 2 PROPERTY OWNERSHIP		
	DESIGNED BY				
	DRAWN BY	SJL 2/89			
	CHECKED BY	GWS 3/89			
	APPROVED BY				
CAD No.	SCALE 1" = 2000'	Job No	Dwg No	REV	



LEGEND

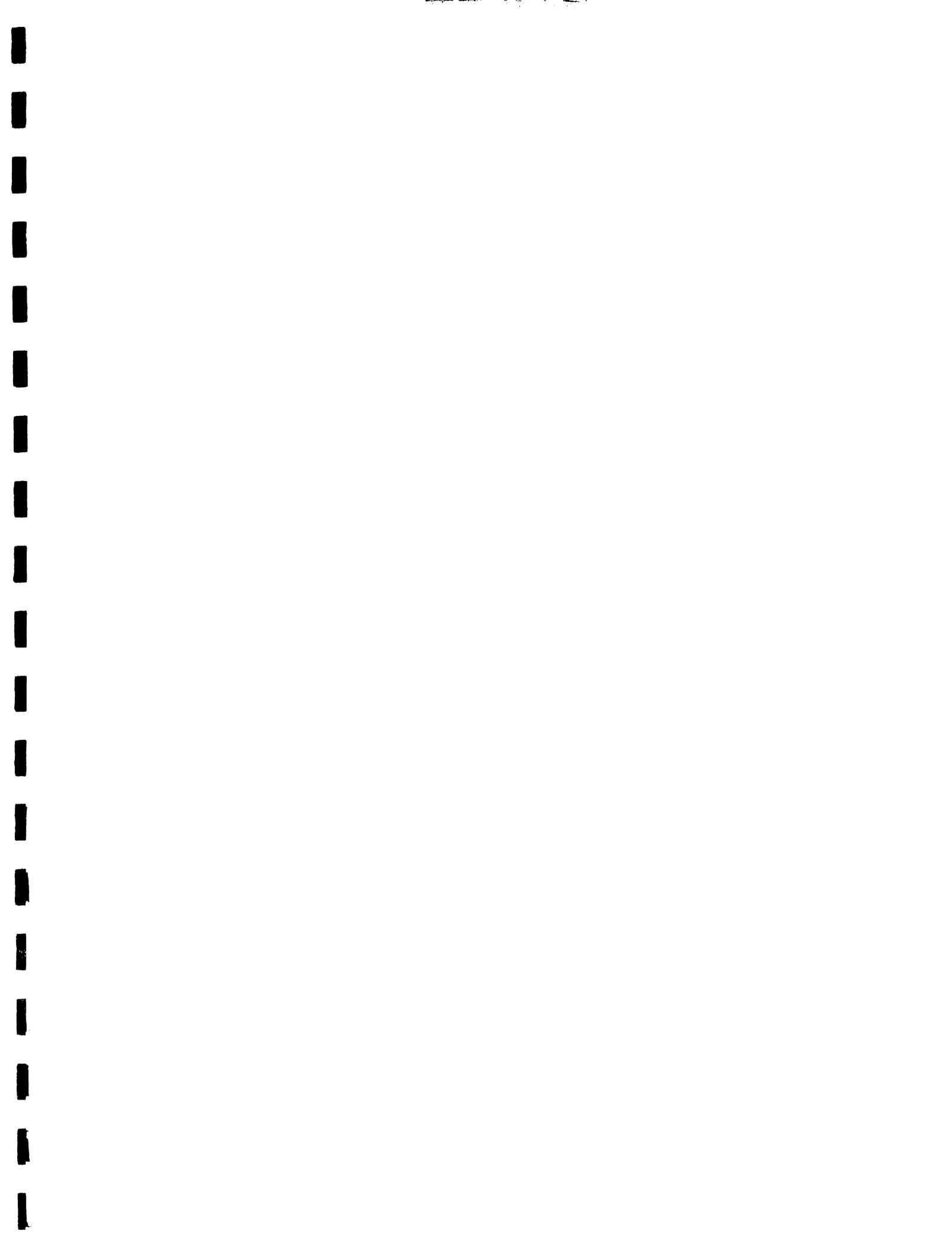
- PRIVATE WELL OWNED BY KENNECOTT
- ⊙ PRIVATE WELL NOT OWNED BY KENNECOTT

— 2 — DRAWDOWN CONTOURS

 ZONE OF DRAWDOWNS > 10'

FOTH & VAN DYKE		
GEOSCIENCES & ENVIRONMENTAL MANAGEMENT DIVISION GREEN BAY, WISCONSIN		
NOTES	APPROVAL	DATE
	DESIGNED BY	
	DRAWN BY R. M. H.	3/89
	CHECKED BY G. W. S.	3/89
	APPROVED BY	
	CAD No.	SCALE 1" = 1000'

KENNECOTT MINERALS COMPANY		
FLAMBEAU PROJECT		
LADYSMITH, WISCONSIN		
FIGURE NO. 5		
INTERPRETATION OF MAXIMUM		
WATER TABLE DRAWDOWN BASED ON		
1983 MODEL SIMULATIONS		
Job No	Dwg No	REV



UW-STEVENS POINT



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